

UNSTEADY CONDUCTIVE HEAT TRANSFER FOR BODIES IN AN INFINITE MEDIUM

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The results are presented of Nusselt number calculations for bodies of different geometrical shape located in an infinite medium, the surface temperature of the bodies being functions of time. A number of particular cases are investigated.

In order to solve various practical problems, we require a description of unsteady heat transfer for bodies of different geometrical shape located in an infinite medium.

Where there is conductive heat transfer with the surrounding medium, and a given law of body surface temperature variation with time, the problem in question reduces to the following differential equation:

$$\frac{\partial \Theta}{\partial \tau} = \frac{\partial^2 \Theta}{\partial \xi^2} + \frac{n}{\xi} \frac{\partial \Theta}{\partial \xi}. \quad (1)$$

The initial conditions are

$$\tau = 0, \Theta = 0. \quad (2)$$

The boundary conditions are

$$\xi = 1, \Theta = \varphi(\tau), \quad (3)$$

$$\xi \rightarrow \infty, \Theta \rightarrow 0. \quad (4)$$

Here $\Theta = (T - T_\infty)/(T_r - T_\infty)$ is temperature; $\tau = at/r^2$ is time; $\xi = x/r$ is a coordinate.

The parameter n , which characterizes the geometry of the system, appears in the problem. With $n = 0; 1; 2$ we have, respectively, an infinite plate of thickness $2r$, a cylinder of infinite length and finite radius, and a sphere.

From the solution of the problem we may then find the heat flux through the body surface ($\xi = 1$), while the external heat transfer is described by the Nusselt number

$$Nu = \frac{\alpha r}{\lambda} = - \frac{1}{\Theta} \frac{\partial \Theta}{\partial \xi} \Big|_{\xi=1}.$$

This problem has been stated in the literature. For instance, in [1], with the help Karman-type integral relations, an approximate expression is derived for calculating the Nusselt number in the sphere case; this has the form

$$Nu = 1 + \frac{1}{\sqrt{3\tau}} \frac{\varphi(\tau)}{\varphi(\tau)},$$

$$\text{where } \bar{\varphi}(\tau) = \left(\int_0^\tau \varphi^2(z) dz / \tau \right)^{1/2}.$$

The method of [1] is very approximate, however, and is used, as will be shown below, only for a bounded class of functions.

In the present paper, for arbitrary type of functions $\varphi(\tau)$ satisfying conditions (2), this problem is solved by the methods of operational calculus.

Leaving out intermediate calculations, the final result has the form

$$n=0, Nu = \frac{1}{\varphi(\tau)} \frac{\partial}{\partial \tau} \int_0^\tau \frac{\varphi(z)}{\sqrt{\pi(\tau-z)}} dz, \quad (5)$$

$$n=1, Nu =$$

$$= \frac{4}{\pi^2 \varphi(\tau)} \frac{\partial}{\partial \tau} \int_0^\tau \varphi(\tau-z) \int_0^\infty \exp(-zu) \frac{dudz}{u [I_0^2(u) + N_0^2(u)]}, \quad (6)$$

$$n=2, Nu = 1 + \frac{1}{\varphi(\tau)} \frac{\partial}{\partial \tau} \int_0^\tau \frac{\varphi(z)}{\sqrt{\pi(\tau-z)}} dz, \quad (7)$$

where I_0 and N_0 are zeroth-order Bessel functions of the first and second kind. The integro-differential relations for the Nusselt number are written in the form of Duhamel integrals [2].

By assigning a definite form of functions $\varphi(\tau)$, we may find the Nusselt number from these relations for each particular case.

Let us examine some examples of one of the simplest cases—spherical symmetry ($n = 2$).

1. Let

$$\varphi(\tau) = k \tau^m, \quad (8)$$

where m is any positive integer. Then, using (7), we have

$$I = \int_0^\tau \frac{(\tau-z)^m}{\sqrt{z}} dz = \tau^{\frac{2m+1}{2}} \left(2 - \frac{m}{1!} \cdot \frac{2}{3} + \frac{m(m-1)}{2!} \cdot \frac{2}{5} + \dots + (-1)^m \frac{2}{2m+1} \right)$$

and

$$Nu = \frac{(2m+1)}{\sqrt{\pi}} \left[1 - \frac{m}{1!} \cdot \frac{1}{3} + \frac{m(m-1)}{2!} \cdot \frac{1}{5} + \dots + (-1)^m \frac{1}{2m+1} \right] \frac{1}{\tau} + 1. \quad (9)$$

From this it follows that, in the case of a power law of surface temperature variation of type (8), for any value of m , the value of Nu is independent of the coefficient of proportionality k , and $\lim_{\tau \rightarrow \infty} Nu = 1$, i.e., steady heat transfer to or from the surrounding medium is possible. We note that the steady heat transfer region sets in earlier (smaller value of τ), the smaller m is.

At the same time, in a given case, we may obtain, by the method of [1],*

$$Nu_1 = 1 + \frac{\sqrt{2m+1}}{\sqrt{3}} \frac{1}{\sqrt{\tau}}$$

or

$$\Delta = \frac{Nu-1}{Nu_1-1} = \frac{\sqrt{2m+1} \sqrt{3}}{\sqrt{\pi}} \times \left[1 - \frac{m}{1!} \cdot \frac{1}{3} + \frac{m(m-1)}{2!} \cdot \frac{1}{5} + \dots + (-1)^m \frac{1}{2m+1} \right],$$

i. e., the error in calculating Nu by the method of [1] increases with increase of m . Calculations show that even for a square law of surface temperature variation ($m = 2$), $\Delta = 55\%$.

2. Let us put

$$\varphi_{(\tau)} = A \sin \omega \tau, \tag{10}$$

i. e., the body surface temperature contains harmonic oscillations of amplitude A and frequency ω . Then the integral

$$I = \int_0^{\tau} \frac{A \sin \omega z}{\sqrt{\pi(\tau-z)}} dz = A \sqrt{\frac{2}{\omega}} [\sin \omega \tau \cdot C_{(\omega\tau)} - \cos \omega \tau \cdot S_{(\omega\tau)}],$$

where $C_{(\omega\tau)} = \sqrt{2/\pi} \int_0^{\sqrt{\omega\tau}} \cos t^2 dt$ and $S_{(\omega\tau)} = \sqrt{2/\pi} \times \int_0^{\sqrt{\omega\tau}} \sin t^2 dt$ are Fresnel integrals.

The heat flux through the body surface $\left. \frac{\partial \Theta}{\partial \xi} \right|_{\xi=1}$ is in this case $\left(\left. \frac{\partial \Theta}{\partial \xi} \right|_{\xi=1} = -Nu \Theta \right)$

$$\left. \frac{\partial \Theta}{\partial \xi} \right|_{\xi=1} = -A [\sin \omega \tau + \sqrt{2\omega} \times (\cos \omega \tau \cdot C_{(\omega\tau)} + \sin \omega \tau \cdot S_{(\omega\tau)})]. \tag{11}$$

For steady oscillations ($\omega\tau \gg 1$) we may put $S_{(\omega\tau)} = C_{(\omega\tau)} = 1/2$, and (11) takes the form

$$\left. \frac{\partial \Theta}{\partial \xi} \right|_{\xi=1} = -A_1 \sin(\omega\tau + \varphi), \tag{12}$$

where $A_1 = A \sqrt{1 + \sqrt{2\omega} + \omega}$ and $\varphi = \arctg(1 + \sqrt{2\omega})$.

When $\omega \gg 2 \arctg(1 + \sqrt{2\omega}) \approx \pi/4$ and $\left. \frac{\partial \Theta}{\partial \xi} \right|_{\xi=1} = -A_1 \sin\left(\frac{\pi}{4} + \omega\tau\right)$.

Thus, in the case of sinusoidal oscillations of body surface temperature, the heat flux also contains harmonic oscillations, but with amplitude A and phase shift φ , dependent on frequency of oscillation ω , i. e., in this case steady heat transfer is impossible.

The Nu number for arbitrary time will have the form

$$Nu = 1 + \sqrt{2\omega} [S_{(\omega\tau)} + \text{ctg } \omega\tau \cdot C_{(\omega\tau)}]. \tag{13}$$

The value of Nu_1 proves to be

$$Nu_1 = 1 + \frac{2\omega \sin \omega\tau}{\sqrt{3}(2\omega\tau - \sin 2\omega\tau)}, \text{ or } \lim_{\omega\tau \rightarrow \infty} Nu_1 = 1,$$

i. e., in this case the method of [1] gives a result that is wrong in principle.

3. Let

$$\varphi_{(\tau)} = \exp \tau - 1. \tag{14}$$

Then

$$I = \int_0^{\tau} \frac{\exp z - 1}{\sqrt{\tau - z}} dz = -2\sqrt{\tau} + \sqrt{\pi} \exp \tau \cdot \text{erf}(\sqrt{\tau}),$$

where $\text{erf}(\sqrt{\tau}) = \frac{2}{\sqrt{\pi}} \int_0^{\sqrt{\tau}} \exp(-t^2) dt$ is the error integral.

The Nu number is

$$Nu = 1 + \frac{\exp \tau}{\exp \tau - 1} \text{erf}(\sqrt{\tau}), \tag{15}$$

or $\lim_{\tau \rightarrow \infty} Nu = 2$.

Thus, in the case of a power law of type (14) for body surface temperature variation, the heat flux, in the limit as $\tau \rightarrow \infty$, is $\left. \frac{\partial \Theta}{\partial \xi} \right|_{\xi=1} = -2\Theta$, i. e., its intensity is twice as large as in steady heat transfer.

By the method of [1] we obtain

$$Nu_1 = 1 + \sqrt{\frac{2}{3}} \frac{\exp \tau - 1}{\sqrt{(\exp \tau - 2)^2 + \tau - 1}} \text{ and } \lim_{\tau \rightarrow \infty} Nu_1 = 1 + \sqrt{\frac{2}{3}} = 1.815,$$

i. e., the error of this method is insignificant ($\sim 9\%$) only at large values of time; at small times it may be appreciable.

* Nu_1 is the value of the parameter calculated by the method of [1].

NOTATION

T - variable temperature; x - coordinate; t - time; T_{∞} - value of temperature when $x \rightarrow \infty$; r - characteristic body dimension; T_r - temperature on body surface; λ - thermal conductivity; a - thermal diffusivity; α - external heat transfer coefficient.

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